

# Effect of reaction scheme on the structure of ammonia turbulent flame

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## I. Abstract

In recent years, global environmental problems, particularly global warming due to carbon dioxide (CO<sub>2</sub>), have become substantially evident. It is therefore necessary to investigate novel and efficient energy utilization methods, to significantly suppress CO<sub>2</sub> emission, and thus preserve the environment. Ammonia (NH<sub>3</sub>) is a fuel that does not emit greenhouse gases. However, the burning velocity of NH<sub>3</sub> is below 0.06 m/s, which is much lower than that of conventional hydrocarbon fuels (oil-based fuels), making it difficult to achieve stable combustion of NH<sub>3</sub>. If NH<sub>3</sub> is forcibly combusted, a large amount of NO<sub>x</sub> (toxic substance) will be generated. In this study, the calculations were performed using three chemical kinetic mechanisms (GRI Mech 3.0, Okafor Mech, Creck Mech), and the best mechanism was selected by comparing the experimental and calculation results. The GRI Mech 3.0 (Smith, et al) has a common reaction that has been used for the combustion calculation of many hydrocarbon fuels. The Okafor Mech (Okafor, et al, 2018) was improved NH<sub>3</sub> reactivity based on GRI Mech 3.0 and Tian Mech. The Creck Mech (Stagni, et al, 2020) was a newly created mechanism and the mechanism for promoting the NH<sub>3</sub>/H<sub>2</sub> reactions was added to the conventional scheme. By comparing the experimental and numerical data (i.e., flame structure and laminar burning velocity), it is found that that the Creck Mech was judged to be the most suitable chemical kinetic mechanism for ammonia burner with hydrogen flame stabilizer.

## II. Results & Discussion

The analysis object of ammonia burner is shown in Figure 1. A stable flame was obtained by separately supplying ammonia, hydrogen, and air in central, duplex, and triple tubes, respectively (Figure 1). The burner developed in this study can supply a high-velocity airflow (8m/s). Figure 2 shows the comparison of flame structure between experimental and numerical result. In particular, NH<sub>3</sub> consumption height from burner rim well agreed, and the distributions of temperature and chemical species by Creck Mech well agreed with experimental result. Figure 3 (a), (b) shows laminar burning velocities  $S_b$  of NH<sub>3</sub>-H<sub>2</sub> (50-50:vol%) /Air flame, and stoichiometric NH<sub>3</sub>-H<sub>2</sub>/Air flame, respectively.  $X_{H_2}$  represents the ratio of H<sub>2</sub> in NH<sub>3</sub>-H<sub>2</sub> mixture fuel. From Figure 3 (a), (b), the Creck Mech can takes account of the improvement of burning velocity and reactivity when H<sub>2</sub> is added to NH<sub>3</sub>.

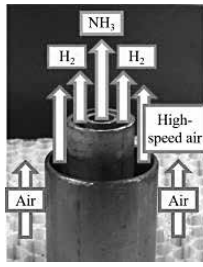


Figure 1. Ammonia burner

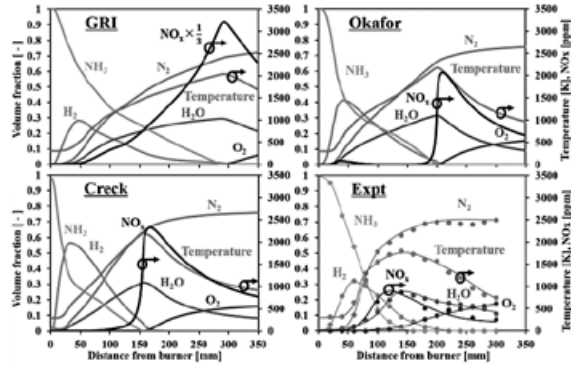


Figure 2. Flame structure at central axes of flame

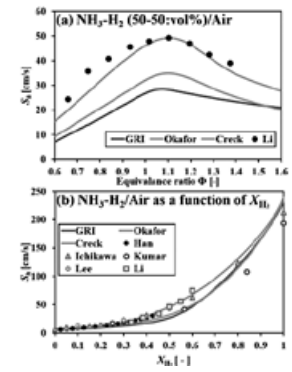


Figure 3. Laminar burning velocity  $S_b$

### III. Conclusion

- (1) From a point of view with the flame structure and laminar burning velocity, the calculation results obtained using the Creck Mech well agreed with the experimental results.
- (2) In GRI Mech 3.0 and Okafor Mech, the flame length became longer because the burning velocity ( $\text{NH}_3/\text{H}_2$ ) due to the addition of  $\text{H}_2$  was not taken into consideration. Then, the GRI Mech 3.0 and Okafor Mech are underestimate reactivity when  $\text{H}_2$  are added to  $\text{NH}_3$ .

### IV. References

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